



**Dynamics and
Real-Time
Simulation
(DARTS)
Laboratory**

Spatial Operator Algebra (SOA)

6. Mass Matrix Inverse

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SOA Foundations Track Topics (serial-chain rigid body systems)



1. **Spatial (6D) notation** – spatial velocities, forces, inertias; spatial cross-product, rigid body transformations & properties; parallel axis theorem
2. **Single rigid body dynamics** – equations of motion about arbitrary frame using spatial notation
3. **Serial-chain kinematics** – minimal coordinate formulation, hinges, velocity recursions, Jacobians; first spatial operators; $O(N)$ scatter and gather recursions
4. **Serial-chain dynamics** – equations of motion using spatial operators; Newton–Euler mass matrix factorization; $O(N)$ inverse dynamics; composite rigid body inertia; forward Lyapunov equation; mass matrix decomposition; mass matrix computation; alternative inverse dynamics
5. **Articulated body inertia** - Concept and definition; Riccati equation; alternative force decompositions
6. **Mass matrix factorization and inversion** – spatial operator identities; Innovations factorization of the mass matrix; Inversion of the mass matrix
7. **Recursive forward dynamics** – $O(N)$ recursive forward dynamics algorithm; including gravity and external forces; inter-body forces identity

See <https://dartslab.jpl.nasa.gov/References/index.php> for publications and references on the SOA methodology.



Recap

Recap



- Developed articulated body model for the decomposition of forces
 - Defined articulated body inertias and related quantities
 - Derived expression for residual forces
 - Developed $O(N)$ gather algorithm for computing these quantities
- Described parallels with estimation theory

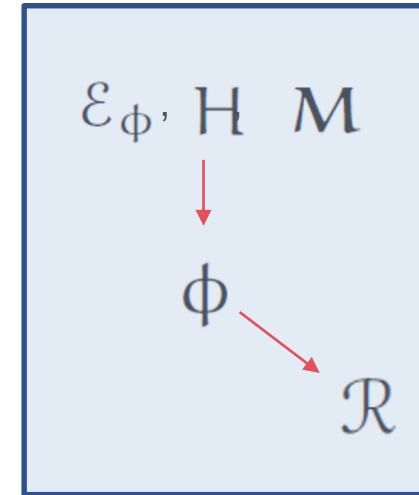


How far have we come?



Spatial operators

- Velocity expression
- Jacobian
- Mass matrix NE factorization
- Lyapunov equation for CRBs
- Mass matrix decomposition



*spatial operators
family*

Have started to build up a vocabulary of spatial operators that can be used to express and manipulate the structure of dynamics quantities.



Recursive Computational Algorithms

- $O(N)$ Gather and scatter recursions pattern
- $O(N)$ Body velocities scatter recursion
- $O(N)$ CRBs gather recursion
- $O(N^2)$ mass matrix computation
- $O(N)$ NE scatter/gather inverse dynamics
- $O(N^2)$ inverse dynamics based mass matrix
- $O(N)$ CRBs based inverse dynamics
- $O(N)$ ATBI gather recursion

Can derive such low-cost scatter/gather algorithms usually by examination of the spatial operator expressions.



Articulated Body Inertia



Inter-body spatial force decompositions

- Force decompositions consist of inertia + residual terms
- From the equations of motion we had

$$f(k) = M(k)\alpha(k) + \phi(k, k - 1)f(k - 1)$$

↑
*depends on
kth body*

↑
depends on all bodies

- Using CRBs we have

$$f(k) = \mathcal{R}(k)\alpha(k) + y(k)$$

↑
*depends on
outboard bodies only*

↑
*depends on outboard
generalized accels*

- Using ATBI we have

$$f(k) = \mathcal{P}(k)\alpha(k) + z(k)$$

↑
*depends on
outboard bodies only*

↑
*depends on outboard
generalized forces*



Defining $\psi(k+1, k)$

Defined the *articulated body transformation matrix*

$$\psi(k+1, k) \triangleq \phi(k+1, k)\bar{\tau}(k)$$

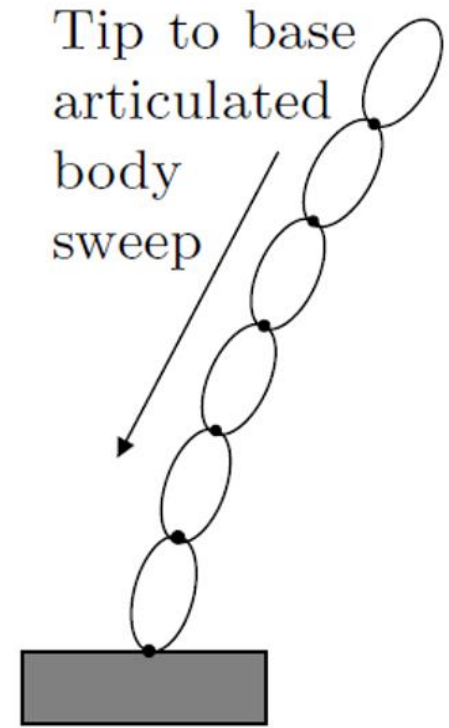
- $\psi(k+1, k)$ is a 6x6 matrix like $\phi(k+1, k)$
- However it is typically singular
- It depends on hinge properties
- Unlike $\phi(k+1, k)$ which propagates across rigid bodies, $\psi(k+1, k)$ propagates across articulated bodies



Articulated body inertias algorithm

$O(N)$ tip-to-base gather algorithm for ATBI quantities

$$\left\{ \begin{array}{l} \mathcal{P}^+(0) = \mathbf{0}, \quad \bar{\tau}(0) = \mathbf{0} \\ \text{for } k \quad 1 \dots n \\ \quad \psi(k, k-1) = \phi(k, k-1)\bar{\tau}(k-1) \\ \quad \mathcal{P}(k) = \phi(k, k-1)\mathcal{P}^+(k-1)\phi^*(k, k-1) + M(k) \\ \quad \mathcal{D}(k) = H(k)\mathcal{P}(k)H^*(k) \\ \quad \mathcal{G}(k) = \mathcal{P}(k)H^*(k)\mathcal{D}^{-1}(k) \\ \quad \mathcal{K}(k+1, k) = \phi(k+1, k)\mathcal{G}(k) \\ \quad \bar{\tau}(k) = \mathbf{I} - \mathcal{G}(k)H(k) \\ \quad \mathcal{P}^+(k) = \bar{\tau}(k)\mathcal{P}(k) \\ \text{end loop} \end{array} \right.$$





Articulated Body Inertia Spatial Operators



ATBI spatial operators

Now define spatial operators using the ATBI quantities

$$\begin{aligned}\mathcal{P} &\triangleq \text{diag} \left\{ \mathcal{P}(\mathbf{k}) \right\}_{\mathbf{k}=1}^n \in \mathcal{R}^{6n \times 6n} \\ \mathcal{D} &\triangleq \text{diag} \left\{ \mathcal{D}(\mathbf{k}) \right\}_{\mathbf{k}=1}^n = \mathbf{H}\mathcal{P}\mathbf{H}^* \in \mathcal{R}^{\mathcal{N} \times \mathcal{N}} \\ \mathcal{G} &\triangleq \text{diag} \left\{ \mathcal{G}(\mathbf{k}) \right\}_{\mathbf{k}=1}^n = \mathcal{P}\mathbf{H}^*\mathcal{D}^{-1} \in \mathcal{R}^{6n \times \mathcal{N}} \\ \mathcal{K} &\triangleq \mathcal{E}_\phi \mathcal{G} \in \mathcal{R}^{6n \times \mathcal{N}} \\ \tau &\triangleq \text{diag} \left\{ \tau(\mathbf{k}) \right\}_{\mathbf{k}=1}^n = \mathcal{G}\mathbf{H} \in \mathcal{R}^{6n \times 6n} \\ \bar{\tau} &\triangleq \text{diag} \left\{ \bar{\tau}(\mathbf{k}) \right\}_{\mathbf{k}=1}^n = \mathbf{I} - \tau \in \mathcal{R}^{6n \times 6n} \\ \mathcal{P}^+ &\triangleq \text{diag} \left\{ \mathcal{P}^+(\mathbf{k}) \right\}_{\mathbf{k}=1}^n = \bar{\tau}\mathcal{P}\bar{\tau}^* = \bar{\tau}\mathcal{P} = \mathcal{P}\bar{\tau}^* \in \mathcal{R}^{6n \times 6n} \\ \mathcal{E}_\psi &\triangleq \mathcal{E}_\phi \bar{\tau} \in \mathcal{R}^{6n \times 6n}\end{aligned}$$



Structure of the \mathcal{K} spatial operator

\mathcal{K} has the same structure as \mathcal{E}_ϕ

$$\mathcal{K} \triangleq \mathcal{E}_\phi \mathcal{G}$$
$$\mathcal{K}(k+1, k) = \phi(k+1, k) \mathcal{G}(k)$$

block diagonal

$$\mathcal{K} = \begin{pmatrix} \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \mathcal{K}(2, 1) & \mathbf{0} & \dots & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \mathcal{K}(3, 2) & \dots & \mathbf{0} & \mathbf{0} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ \mathbf{0} & \mathbf{0} & \dots & \mathcal{K}(n, n-1) & \mathbf{0} \end{pmatrix}$$

Only non-zero entries are along the first sub-diagonal



Structure of \mathcal{E}_ψ

\mathcal{E}_ψ also has the same structure as \mathcal{E}_ϕ

$$\mathcal{E}_\psi \triangleq \mathcal{E}_\phi \bar{\tau}$$

$$\psi(k+1, k) \triangleq \phi(k+1, k) \bar{\tau}(k)$$

block diagonal

$$\mathcal{E}_\psi = \begin{pmatrix} \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} & \mathbf{0} \\ \psi(2, 1) & \mathbf{0} & \dots & \mathbf{0} & \mathbf{0} \\ \mathbf{0} & \psi(3, 2) & \dots & \mathbf{0} & \mathbf{0} \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ \mathbf{0} & \mathbf{0} & \dots & \psi(n, n-1) & \mathbf{0} \end{pmatrix}$$

\mathcal{E}_ψ has same structure as \mathcal{E}_ϕ



Like \mathcal{E}_ϕ , \mathcal{E}_ψ is nilpotent

$$\mathcal{E}_\psi = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ \psi(2,1) & 0 & \dots & 0 & 0 \\ 0 & \psi(3,2) & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & \psi(n,n-1) & 0 \end{pmatrix}$$

$$\mathcal{E}_\psi \triangleq \mathcal{E}_\phi \bar{\tau}$$

- Every power of \mathcal{E}_ψ results in a matrix with the sub-diagonal shifted one step lower

$$\mathcal{E}_A = \begin{pmatrix} \cdot & \cdot & \cdot & \cdot \\ X & \cdot & \cdot & \cdot \\ \cdot & X & \cdot & \cdot \\ \cdot & \cdot & X & \cdot \end{pmatrix}, \mathcal{E}_A^2 = \begin{pmatrix} \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ X & \cdot & \cdot & \cdot \\ \cdot & X & \cdot & \cdot \end{pmatrix}, \mathcal{E}_A^3 = \begin{pmatrix} \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ \cdot & \cdot & \cdot & \cdot \\ X & \cdot & \cdot & \cdot \end{pmatrix}$$

- At the nth power, the result is zero: $\mathcal{E}_\psi^n = \mathbf{0}$
- Hence \mathcal{E}_ψ is nilpotent!



Structural properties of \mathcal{E}_ψ

- Strictly lower triangular, square, singular and nilpotent,
- Only the first sub-diagonal has nonzero elements
- The non-zero entries are the **configuration dependent** 6x6 inter-link articulated body transformation matrices (configuration dependent)

$$\mathcal{E}_\psi = \begin{pmatrix} 0 & 0 & 0 & 0 & 0 \\ \psi(2,1) & 0 & \dots & 0 & 0 \\ 0 & \psi(3,2) & \dots & 0 & 0 \\ \vdots & \vdots & \ddots & \vdots & \vdots \\ 0 & 0 & \dots & \psi(n, n-1) & 0 \end{pmatrix}$$



Recall: Nilpotent matrices & inverses

- A square matrix \mathbf{U} is said to be nilpotent if one of its powers becomes 0, i.e. if for some n

$$\mathbf{U}^n = \mathbf{0}$$

- For a nilpotent \mathbf{U} , we have

$$(\mathbf{I} - \mathbf{U})^{-1} = \mathbf{I} + \mathbf{U} + \mathbf{U}^2 + \dots + \mathbf{U}^{n-1}$$

1-resolvent

*Series expansion truncates after only a **finite** number of terms for nilpotent matrix, hence the 1-resolvent inverse is well defined*

ψ Is the 1-resolvent of \mathcal{E}_ψ



Analogous to

$$\phi \triangleq (\mathbf{I} - \mathcal{E}_\phi)^{-1} = \mathbf{I} + \mathcal{E}_\phi + \mathcal{E}_\phi^2 + \dots + \mathcal{E}_\phi^{n-1}$$

$$\phi(i, j) = \phi(i, i-1) \dots \phi(j+1, j)$$

define

$$\psi \triangleq (\mathbf{I} - \mathcal{E}_\psi)^{-1} = \mathbf{I} + \mathcal{E}_\psi + \mathcal{E}_\psi^2 + \dots + \mathcal{E}_\psi^{n-1}$$

$$= \begin{pmatrix} \mathbf{I} & \mathbf{0} & \dots & \mathbf{0} \\ \psi(2, 1) & \mathbf{I} & \dots & \mathbf{0} \\ \vdots & \vdots & \ddots & \vdots \\ \psi(n, 1) & \psi(n, 2) & \dots & \mathbf{I} \end{pmatrix}$$

$$\psi(i, j) \triangleq \psi(i, i-1) \dots \psi(j+1, j) \quad \text{for } i > j$$

$\tilde{\psi}$

Spatial operator



Analogous to

$$\tilde{\phi} \triangleq \phi - \mathbf{I}$$

*Same as ϕ , except
diagonal elements are now
zero matrices*

and

$$\tilde{\phi} = \mathcal{E}_{\phi} \phi = \phi \mathcal{E}_{\phi}$$

define

$$\tilde{\psi} \triangleq \psi \mathcal{E}_{\psi} = \mathcal{E}_{\psi} \psi = \psi - \mathbf{I}$$

*Same as ψ , except
diagonal elements are now
zero matrices*



Articulated vs Composite Body Models

Comparison of composite and articulated body models



Variable	Composite Body	Articulated Body
Relative hinge acceleration α $\alpha(k)$ α with respect to α^+	$\ddot{\theta}$ $\phi^* H^* \ddot{\theta}$ $\phi^*(k+1, k)\alpha(k+1) + H^*(k)\ddot{\theta}(k)$ $\alpha^+ + H^* \ddot{\theta}$	v $\psi^* H^* v$ $\psi^*(k+1, k)\alpha(k+1) + H^*(k)v(k)$ $\bar{\tau}^* \alpha^+ + H^* v$ $(\bar{\tau}^* \alpha = \bar{\tau}^* \alpha^+)$
v	$\mathcal{G}^* \alpha^+ + \ddot{\theta}$	$\mathcal{G}^* \alpha$
Effective inertia Relationship to M	\mathcal{R} $\mathcal{R} - \mathcal{E}_\phi \mathcal{R} \mathcal{E}_\phi^*$	\mathcal{P} $\mathcal{P} - \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^*$
Inertia recursions	$\mathcal{R}^+(k) = \mathcal{R}(k)$ $\mathcal{R}(k+1) = \phi(k+1, k)\mathcal{R}^+(k)\phi^*(k+1, k) + M(k)$	$\mathcal{P}^+(k+1) = \bar{\tau}(k)\mathcal{P}(k)\bar{\tau}^*(k)$ $\mathcal{P}(k+1) = \phi(k+1, k)\mathcal{P}^+(k)\phi^*(k+1, k) + M(k)$
f on (- side) Correction force (- side)	$\mathcal{R}\alpha + y$ $y = \tilde{\phi} \mathcal{R} H^* \ddot{\theta}$	$\mathcal{P}\alpha + z$ $z = \tilde{\phi} \mathcal{P} H^* v$
f on + side Correction force (+ side)	$\mathcal{R}^+ \alpha^+ + y^+$ $y^+ = y + \mathcal{R} H^* \ddot{\theta}$	$\mathcal{P}^+ \alpha^+ + z^+$ $z^+ = z + \mathcal{P} H^* v$



**Scatter Recursions for
as for**

same

ψ

ϕ

Recall: Base-to-tips structure-based O(N) scatter recursion for ϕ



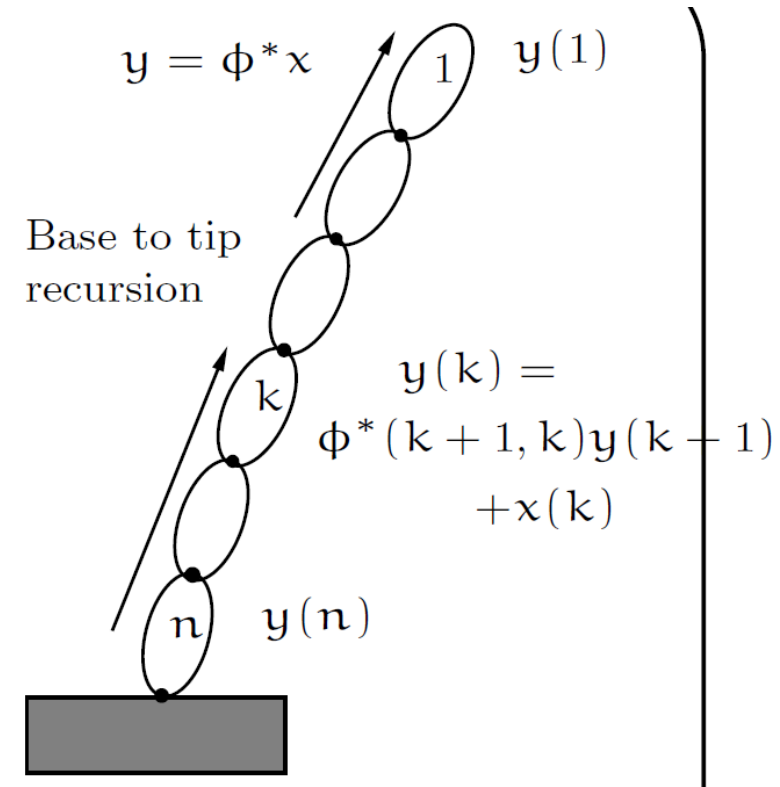
operator transpose/vector product

$$y = \phi^* x$$



- Applies to any x
- Does not require explicit computation of ϕ at all
- Only depends on elements of \mathcal{E}_ϕ

$$\left\{ \begin{array}{l} y(n+1) = 0 \\ \text{for } k \quad n \cdots 1 \\ \quad y(k) = \phi^*(k+1, k)y(k+1) + x(k) \\ \text{end loop} \end{array} \right.$$



Algorithm flow

Example – link velocity computation

O(N) structure-based, base-to-tip scatter recursion

Generalized base-to-tips structure-based scatter recursion



operator transpose/vector product

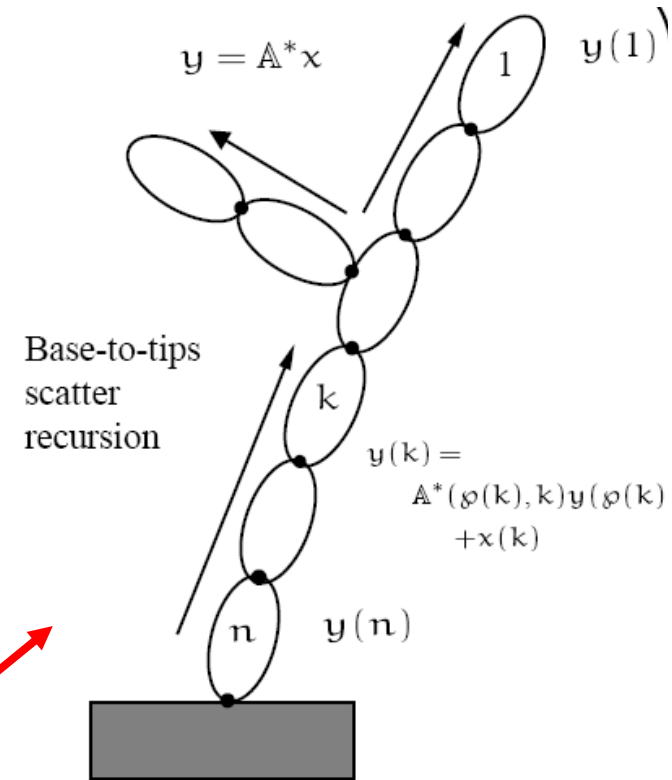
$$y = A^* x$$

$$A = \phi, \psi$$

- Applies to any x
- Does not require explicit computation of A at all
- Only depends on elements of \mathcal{E}_A

{ for all nodes k (base-to-tips scatter)
 $y(k) = A^*(\rho(k), k)y(\rho(k)) + x(k)$
 } end loop

O(N) structure-based scatter algorithm



Algorithm flow



Gather Recursions for ψ same as for ϕ

Recall: Tips-to-base structure-based $O(N)$ gather recursion for ϕ



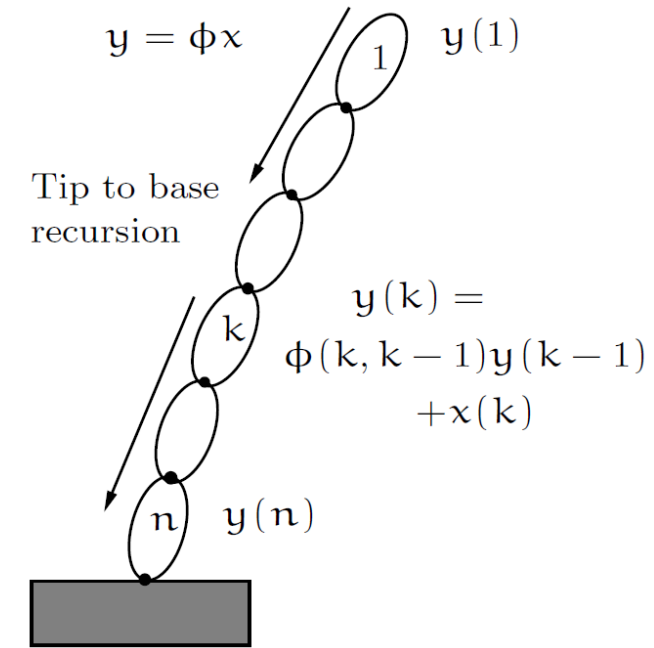
operator/vector product

$$y = \phi x$$



- Applies to any x
- Does not require explicit computation of ϕ at all
- Only depends on elements of \mathcal{E}_ϕ

$$\left\{ \begin{array}{l} y(0) = 0 \\ \text{for } k \quad 1 \cdots n \\ \quad y(k) = \phi(k, k-1)y(k-1) + x(k) \\ \text{end loop} \end{array} \right.$$



Algorithm flow

$O(N)$ structure-based tip-to-base gather recursion

Example – torque for end-effector force

Generalized tips-to-base structure-based gather recursion



operator/vector product

$$y = Ax$$

$$A = \phi, \psi$$

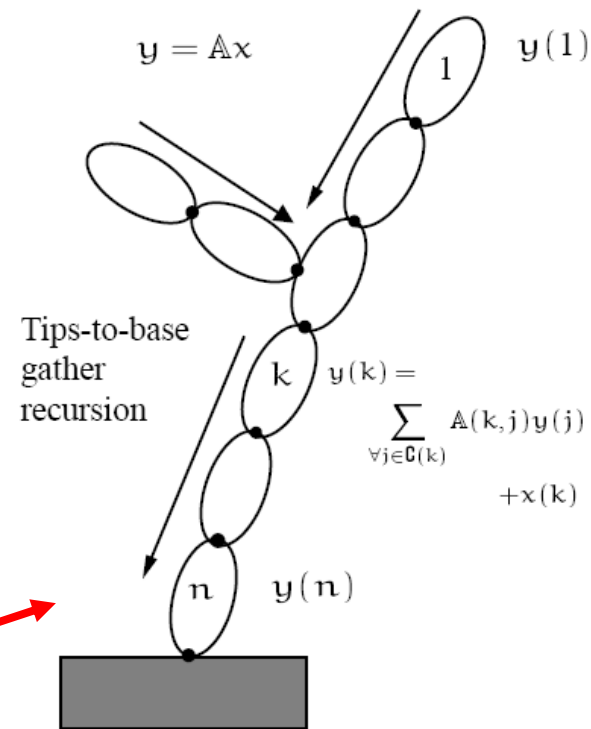


- Applies to any x
- Does not require explicit computation of A at all
- Only depends on elements of \mathcal{E}_A

for all nodes k (tips-to-base gather)

$$y(k) = \sum_{\forall i \in \mathcal{C}(k)} A(k, i)y(i) + x(k)$$

end loop



Algorithm flow

O(N) structure-based gather algorithm



ATBI Riccati Equation



Recall: Forward Lyapunov Equation for CRBs

CRB recursion

$$\mathcal{R}(k) = \phi(k, k-1)\mathcal{R}(k-1)\phi^*(k, k-1) + \mathcal{M}(k)$$

Define CRB spatial operator

$$\mathcal{R} \triangleq \text{diag} \left\{ \mathcal{R}(k) \right\}_{k=1}^n \in \mathcal{R}^{6n \times 6n}$$

Can re-express as CRB “forward Lyapunov equation” using spatial operators

$$\mathbf{M} = \mathcal{R} - \mathcal{E}_\phi \mathcal{R} \mathcal{E}_\phi^*$$



Riccati equation for ATBI

Similar to Lyapunov equation

$$\mathbf{M} = \mathcal{R} - \mathcal{E}_\phi \mathcal{R} \mathcal{E}_\phi^*$$

The ATBI recursion

$$\mathcal{P}(k+1) \stackrel{6.32}{=} \psi(k+1, k) \mathcal{P}(k) \psi^*(k+1, k) + \mathbf{M}(k+1)$$

can be re-expressed at the operator level as

$$\mathbf{M} = \mathcal{P} - \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^* = \mathcal{P} - \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\phi^*$$



ATBI operator identity

Claim:

$$\mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^* = \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\phi^*$$

Derivation:

Have $\mathcal{P}(\mathbf{k}) \bar{\tau}^*(\mathbf{k}) = \bar{\tau}(\mathbf{k}) \mathcal{P}(\mathbf{k}) = \bar{\tau}(\mathbf{k}) \mathcal{P}(\mathbf{k}) \bar{\tau}^*(\mathbf{k})$

$$\mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^* \stackrel{7.3}{=} \mathcal{E}_\psi \mathcal{P} \bar{\tau}^* \mathcal{E}_\phi^* \stackrel{7.3}{=} \mathcal{E}_\psi \bar{\tau} \mathcal{P} \mathcal{E}_\phi^* \stackrel{7.3}{=} \mathcal{E}_\phi \bar{\tau} \bar{\tau} \mathcal{P} \mathcal{E}_\phi^* = \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\phi^*$$



Recall: Operator decomposition of $\phi M \phi^*$

Claim:

$$\phi M \phi^* = \mathcal{R} + \tilde{\phi} \mathcal{R} + \mathcal{R} \tilde{\phi}^*$$

Derivation:

$$M = \mathcal{R} - \mathcal{E}_\phi \mathcal{R} \mathcal{E}_\phi^*$$

and thus pre & post multiplying

use identity

$$\tilde{\phi} \triangleq \phi - \mathbf{I} = \mathcal{E}_\phi \phi$$

$$\begin{aligned} \phi M \phi^* &\stackrel{4.9}{=} \phi \mathcal{R} \phi^* - \phi \mathcal{E}_\phi \mathcal{R} \mathcal{E}_\phi^* \phi^* \stackrel{3.41}{=} \phi \mathcal{R} \phi^* - \tilde{\phi} \mathcal{R} \tilde{\phi}^* \\ &\stackrel{3.40}{=} (\tilde{\phi} + \mathbf{I}) \mathcal{R} (\tilde{\phi} + \mathbf{I}) - \tilde{\phi} \mathcal{R} \tilde{\phi}^* \stackrel{3.40}{=} \mathcal{R} + \tilde{\phi} \mathcal{R} + \mathcal{R} \tilde{\phi}^* \end{aligned}$$



Operator decomposition of $\psi \mathbf{M} \psi^*$

Previously $\phi \mathbf{M} \phi^* = \mathcal{R} + \tilde{\phi} \mathcal{R} + \mathcal{R} \tilde{\phi}^*$

Claim:

disjoint decomposition

$$\psi \mathbf{M} \psi^* = \mathcal{P} + \tilde{\psi} \mathcal{P} + \mathcal{P} \tilde{\psi}^*$$

block-diagonal

strictly lower triangular

strictly upper triangular

Derivation:

use $\mathbf{M} = \mathcal{P} - \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^*$

$$\begin{aligned} \psi \mathbf{M} \psi^* &= \psi \mathcal{P} \psi^* - \psi \mathcal{E}_\psi \mathcal{P} \mathcal{E}_\psi^* \psi^* \stackrel{7.8}{=} (\tilde{\psi} + \mathbf{I}) \mathcal{P} (\tilde{\psi} + \mathbf{I})^* - \tilde{\psi} \mathcal{P} \tilde{\psi}^* \\ &= \mathcal{P} + \tilde{\psi} \mathcal{P} + \mathcal{P} \tilde{\psi}^* \end{aligned}$$

$$\tilde{\psi} \triangleq \psi \mathcal{E}_\psi = \mathcal{E}_\psi \psi = \psi - \mathbf{I}$$

use identity



Operator Identities

Identities relating ϕ , ψ



Now we will establish a sequence of identities that illustrate a close relationship between the ϕ , ψ spatial operators.



Identity: $\psi^{-1} - \phi^{-1} = \mathcal{KH}$

Claim:

$$\psi^{-1} - \phi^{-1} = \mathcal{KH}$$

Derivation:

$$\tau = \mathcal{GH}$$

$$\begin{aligned} \psi^{-1} &= \mathbf{I} - \mathcal{E}_\psi \stackrel{7.3}{=} \mathbf{I} - \mathcal{E}_\phi \bar{\tau} \stackrel{7.3}{=} (\mathbf{I} - \mathcal{E}_\phi) + \mathcal{E}_\phi \tau \\ &\stackrel{3.36, 7.3}{=} \phi^{-1} + \mathcal{E}_\phi \mathcal{GH} \stackrel{7.3}{=} \phi^{-1} + \mathcal{KH} \end{aligned}$$



More identities

Claim:

$$\psi^{-1}\phi = \mathbf{I} + \mathcal{K}\mathbf{H}\phi$$

$$\phi\psi^{-1} = \mathbf{I} + \phi\mathcal{K}\mathbf{H}$$

$$\phi^{-1}\psi = \mathbf{I} - \mathcal{K}\mathbf{H}\psi$$

$$\psi\phi^{-1} = \mathbf{I} - \psi\mathcal{K}\mathbf{H}$$

Derivation:

These follow by pre & post multiplying the following identity by ϕ , ψ

$$\psi^{-1} - \phi^{-1} = \mathcal{K}\mathbf{H}$$



... and some more identities

Claim:

$$[\mathbf{I} - \mathbf{H}\psi\mathcal{K}]\mathbf{H}\phi = \mathbf{H}\psi$$

$$\phi\mathcal{K}[\mathbf{I} - \mathbf{H}\psi\mathcal{K}] = \psi\mathcal{K}$$

$$[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]\mathbf{H}\psi = \mathbf{H}\phi$$

$$\psi\mathcal{K}[\mathbf{I} + \mathbf{H}\phi\mathcal{K}] = \phi\mathcal{K}$$

Derivation:

For the first identity,

use identity

$$\psi\phi^{-1} = \mathbf{I} - \psi\mathcal{K}\mathbf{H}$$

$$[\mathbf{I} - \mathbf{H}\psi\mathcal{K}]\mathbf{H}\phi = \mathbf{H}[\mathbf{I} - \psi\mathcal{K}\mathbf{H}]\phi \stackrel{7.11}{=} \mathbf{H}(\psi\phi^{-1})\phi = \mathbf{H}\psi$$



Identities recap

$$\psi^{-1} - \phi^{-1} = \mathcal{K}\mathcal{H}$$

$$\psi^{-1}\phi = \mathbf{I} + \mathcal{K}\mathcal{H}\phi$$

$$\phi\psi^{-1} = \mathbf{I} + \phi\mathcal{K}\mathcal{H}$$

$$\phi^{-1}\psi = \mathbf{I} - \mathcal{K}\mathcal{H}\psi$$

$$\psi\phi^{-1} = \mathbf{I} - \psi\mathcal{K}\mathcal{H}$$

$$[\mathbf{I} - \mathcal{H}\psi\mathcal{K}]\mathcal{H}\phi = \mathcal{H}\psi$$

$$\phi\mathcal{K}[\mathbf{I} - \mathcal{H}\psi\mathcal{K}] = \psi\mathcal{K}$$

$$[\mathbf{I} + \mathcal{H}\phi\mathcal{K}]\mathcal{H}\psi = \mathcal{H}\phi$$

$$\psi\mathcal{K}[\mathbf{I} + \mathcal{H}\phi\mathcal{K}] = \phi\mathcal{K}$$

These identities are very useful in transforming and simplifying operator expressions. We will see their use in a number of instances ahead.



Identity

$$H\psi M\psi^*H^* = \mathcal{D}$$



Expression for $H\psi M\psi^*H^*$

Claim:

$$H\psi M\psi^*H^* = \mathcal{D}$$

Derivation:

$$\begin{aligned} H\psi M\psi^*H^* &\stackrel{7.7}{=} H(\mathcal{P} + \tilde{\psi}\mathcal{P} + \mathcal{P}\tilde{\psi}^*)H^* \stackrel{7.3}{=} \mathcal{D} + H\tilde{\psi}\mathcal{P}H^* + H\mathcal{P}\tilde{\psi}^*H^* \\ &\stackrel{7.8}{=} \mathcal{D} + H\psi\mathcal{E}_\psi\mathcal{P}H^* + H\mathcal{P}\mathcal{E}_\psi^*\psi^*H^* \\ &\stackrel{7.3}{=} \mathcal{D} + H\psi\mathcal{E}_\phi\bar{\tau}\mathcal{P}H^* + H\mathcal{P}\bar{\tau}^*\mathcal{E}_\phi^*\psi^*H^* \\ &\stackrel{7.3}{=} \mathcal{D} + H\psi\mathcal{E}_\phi\mathcal{P}^+H^* + H\mathcal{P}^+\mathcal{E}_\phi^*\psi^*H^* \\ &\stackrel{6.28}{=} \mathcal{D} \end{aligned}$$



Comparison of operator expressions

Earlier mass matrix expression

$$\mathcal{M}(\theta) \triangleq \mathbf{H}\phi\mathbf{M}\phi^*\mathbf{H}^* \quad \text{dense}$$

versus similar expression

block-diagonal

$$\mathbf{H}\psi\mathbf{M}\psi^*\mathbf{H}^* = \mathcal{D}$$

Complex product of spatial operators collapses into just \mathcal{D} !

The only difference is the use of ψ instead of ϕ !



Mass Matrix Innovations Factorization

Recall: The Newton-Euler Factorization of the mass matrix $\mathcal{M}(\theta)$



$$\mathcal{M}(\theta) \triangleq \mathbf{H}\phi\mathbf{M}\phi^*\mathbf{H}^*$$

- Square, symmetric and positive definite
- Size is the number of degrees of freedom
- The mass matrix is configuration dependent
- Dense matrix for serial chain systems
 - key reason for its perceived “complexity”
- Maps generalized velocities to system kinetic energy
- **Not** all of the operators in the Newton-Euler factorization of the mass matrix are **square**
 - Will encounter other factorizations with square factors
- Elements of $\phi^*\mathbf{H}^*$ are Kane’s partial velocities



Innovations Factorization of the mass matrix $\mathcal{M}(\theta)$

Claim:

Innovations Factorization

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}] \mathcal{D} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

Derivation:

use identity

$$[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]\mathbf{H}\psi = \mathbf{H}\phi$$

$$\begin{aligned} \mathcal{M} &\stackrel{5.25}{=} \mathbf{H}\phi\mathbf{M}\phi^*\mathbf{H}^* = \mathbf{H}(\phi\psi^{-1})\psi\mathbf{M}\psi^*(\phi\psi^{-1})^*\mathbf{H}^* \\ &\stackrel{7.11}{=} \mathbf{H}[\mathbf{I} + \phi\mathcal{K}\mathbf{H}]\psi\mathbf{M}\psi^*[\mathbf{I} + \phi\mathcal{K}\mathbf{H}]^*\mathbf{H}^* \\ &= [\mathbf{I} + \mathbf{H}\phi\mathcal{K}](\mathbf{H}\psi\mathbf{M}\psi^*\mathbf{H}^*)[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^* \stackrel{7.13}{=} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]\mathcal{D}[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^* \end{aligned}$$

USE identity

$$\mathbf{H}\psi\mathbf{M}\psi^*\mathbf{H}^* = \mathcal{D}$$



Properties of the Innovations Factorization of the mass matrix

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}] \mathcal{D} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

*Lower triangular with
identity along block-
diagonal*

Block-diagonal

*Upper triangular with
identity along block-
diagonal*

- In the Newton-Euler factorization of the mass matrix, not all the factors were square
- However all the factors are square in the Innovations Factorization
- Moreover, the factors have block-triangular and block-diagonal structure
- And as we will see, they are easy to invert!



Implications for forward dynamics

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}] \mathcal{D} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

*Lower triangular with
identity along block-
diagonal*

Block-diagonal

*Upper triangular with
identity along block-
diagonal*

- Forward dynamics involves computing $\ddot{\theta} = \mathcal{M}^{-1}(\mathcal{T} - \mathcal{C})$
With the NE factorization our options were limited to $O(\mathcal{N}^3)$
complexity
- The new factors however can be computed at $O(\mathcal{N}^2)$ cost
- More these factors can be used to compute $\ddot{\theta} = \mathcal{M}^{-1}(\mathcal{T} - \mathcal{C})$
at $O(\mathcal{N}^2)$ cost as well.
- This is progress - exploitation of the underlying structure
has reduced computational costs – again!



Recall: Trace of the mass matrix

$$\mathcal{M} = \mathbf{H}\mathcal{R}\mathbf{H}^* + \mathbf{H}\tilde{\phi}\mathcal{R}\mathbf{H}^* + \mathbf{H}\mathcal{R}\tilde{\phi}^*\mathbf{H}^*$$

zero trace

General expression

$$\text{Trace}\{\mathcal{M}(\theta)\} = \sum_{i=1}^n \text{Trace}\{\mathbf{H}(\mathbf{k})\mathcal{R}(\mathbf{k})\mathbf{H}^*(\mathbf{k})\}$$

For 1 dof hinges

$$\text{Trace}\{\mathbf{H}(\mathbf{k})\mathcal{R}(\mathbf{k})\mathbf{H}^*(\mathbf{k})\} = \mathbf{H}(\mathbf{k})\mathcal{R}(\mathbf{k})\mathbf{H}^*(\mathbf{k})$$



Determinant of the mass matrix

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}] \mathcal{D} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

Lower triangular with identity along block-diagonal

Block-diagonal

Upper triangular with identity along block-diagonal

determinant 1

The determinant of a matrix is the product of the determinant of its square factors

General expression

$$\det \{\mathcal{M}\} = \prod_{k=1}^n \det \{\mathcal{D}(k)\}$$

scalar for 1 dof hinge



Application of mass matrix determinant: Fixman Potential

The Fixman potential is needed in molecular dynamics simulations for correcting statistical biases

$$U_f \triangleq \log\{\det\{\mathcal{M}\}\}$$

Computing and using it has been an intractable problem for decades

$$\prod_{k=1}^n \det\{\mathcal{D}(k)\}$$

$$\frac{\partial \log\{\det\{\mathcal{M}\}\}}{\partial \theta_i} = 2 \text{Trace} \left\{ \mathcal{P}(i) \Upsilon(i) \tilde{H}^*(i) \right\}$$

Torque from the Fixman potential

Available from standard ATBI computations

Explicit simple expression via SOA for longstanding intractable problem.



More operator decompositions



Decomposition of $\phi M \psi^*$

Previously $\psi M \psi^* = \mathcal{P} + \tilde{\psi} \mathcal{P} + \mathcal{P} \tilde{\psi}^*$

Claim:

$$\phi M \psi^* = \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\psi}^*$$

block-diagonal

strictly lower triangular

strictly upper triangular

Derivation:

Have $M = \mathcal{P} - \mathcal{E}_\phi \mathcal{P} \mathcal{E}_\psi^*$

Pre and post multiply by ϕ, ψ to get

$$\begin{aligned} \phi M \psi^* &\stackrel{3.41, 7.8}{=} \phi \mathcal{P} \psi^* - \tilde{\phi} \mathcal{P} \tilde{\psi}^* = (\tilde{\phi} + \mathbf{I}) \mathcal{P} (\tilde{\psi}^* + \mathbf{I}) - \tilde{\phi} \mathcal{P} \tilde{\psi}^* \\ &= \tilde{\phi} \mathcal{P} \tilde{\psi}^* + \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\psi}^* - \tilde{\phi} \mathcal{P} \tilde{\psi}^* = \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\psi}^* \end{aligned}$$



Another decomposition of $\phi M \phi^*$

Previously

$$\phi M \phi^* = \mathcal{R} + \tilde{\phi} \mathcal{R} + \mathcal{R} \tilde{\phi}^*$$

using CRBs

Claim:

using ATBIs

$$\phi M \phi^* = \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\phi}^* + \phi \mathcal{K} \mathcal{D} \mathcal{K}^* \phi^*$$

block-diagonal

strictly lower triangular

strictly upper triangular

dense

Derivation:

$$\phi M \phi^* = (\phi \psi^{-1}) \psi M \phi^* \stackrel{7.15}{=} (\phi \psi^{-1}) [\psi \mathcal{P} + \mathcal{P} \tilde{\phi}^*]$$

$$\stackrel{7.11}{=} \phi \mathcal{P} + [\mathbf{I} + \phi \mathcal{K} \mathcal{H}] \mathcal{P} \tilde{\phi}^* = \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\phi}^* + \phi \mathcal{K} \mathcal{H} \mathcal{P} \mathcal{E}_\phi^* \phi^*$$

$$\stackrel{6.13}{=} \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\phi}^* + \phi \mathcal{K} \mathcal{D} \mathcal{G}^* \mathcal{E}_\phi^* \phi^* \stackrel{6.36}{=} \mathcal{P} + \tilde{\phi} \mathcal{P} + \mathcal{P} \tilde{\phi}^* + \phi \mathcal{K} \mathcal{D} \mathcal{K}^* \phi^*$$

This is an alternative decomposition using ATBIs.



CRB vs ATBI comparison

Claim:

$$\mathcal{R} \geq \mathcal{P}$$

SHOW!

*Hint: use results
on previous slide*



Inversion of the Mass Matrix



Inverting the mass matrix $\mathcal{M}(\theta)$

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}] \mathcal{D} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

*Lower triangular with
identity along block-
diagonal*

Block-diagonal

*Upper triangular with
identity along block-
diagonal*

- All the factors are square in the Innovations Factorization
- So want to look into inverting the mass matrix by inverting its factors
- \mathcal{D} is block-diagonal, and easy to invert
- We will thus focus on inverting $[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]$



Inverse of $[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]$

Claim:

$$[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-1} = [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]$$

*Lower triangular with identity
along block-diagonal*

Derivation:

Have general matrix identity

$$(\mathbf{I} + \mathbf{A}\mathbf{B})^{-1} = \mathbf{I} - \mathbf{A}(\mathbf{I} + \mathbf{B}\mathbf{A})^{-1}\mathbf{B}$$

$$\begin{aligned} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-1} &= \mathbf{I} - \mathbf{H}[\mathbf{I} + \phi\mathcal{K}\mathbf{H}]^{-1}\phi\mathcal{K} \stackrel{7.11}{=} \mathbf{I} - \mathbf{H}(\phi\psi^{-1})^{-1}\phi\mathcal{K} \\ &= \mathbf{I} - \mathbf{H}\psi\mathcal{K} \end{aligned}$$

using

$$\phi\psi^{-1} = \mathbf{I} + \phi\mathcal{K}\mathbf{H}$$



Mass matrix inverse

Claim:

$$\mathcal{M}^{-1} = [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]^* \mathcal{D}^{-1} [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]$$

Derivation:

$$\begin{aligned} \mathcal{M}^{-1} &\stackrel{7.14}{=} \{[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]\mathcal{D}[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*\}^{-1} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-*} \mathcal{D}^{-1} [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-1} \\ &\stackrel{7.4}{=} [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]^* \mathcal{D}^{-1} [\mathbf{I} - \mathbf{H}\psi\mathcal{K}] \end{aligned}$$

using

$$[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-1} = [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]$$



Comments on mass matrix inverse

$$\mathcal{M}^{-1} = [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]^* \mathcal{D}^{-1} [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]$$

*Upper triangular with
identity along block-
diagonal*

Block-diagonal

*Lower triangular with
identity along block-
diagonal*

- Analytical, closed-form expression for the mass matrix using spatial operators
- The factors are square and invertible – and have diagonal and triangular structure
- The expression is valid for any size system and branching structure



Progression with the Mass Matrix

$$\mathcal{M} = \mathbf{H}\phi\mathbf{M}\phi^*\mathbf{H}^*$$

Analytical Newton-Euler
factorization of the mass matrix

$$\mathcal{M} = [\mathbf{I} + \mathbf{H}\phi\mathcal{K}]\mathcal{D}[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^*$$

Analytical Innovations
factorization of the mass
matrix

$$[\mathbf{I} + \mathbf{H}\phi\mathcal{K}]^{-1} = \mathbf{I} - \mathbf{H}\psi\mathcal{K}$$

$$\mathcal{M}^{-1} = [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]^* \mathcal{D}^{-1} [\mathbf{I} - \mathbf{H}\psi\mathcal{K}]$$

Analytical operator expression for the mass matrix inverse



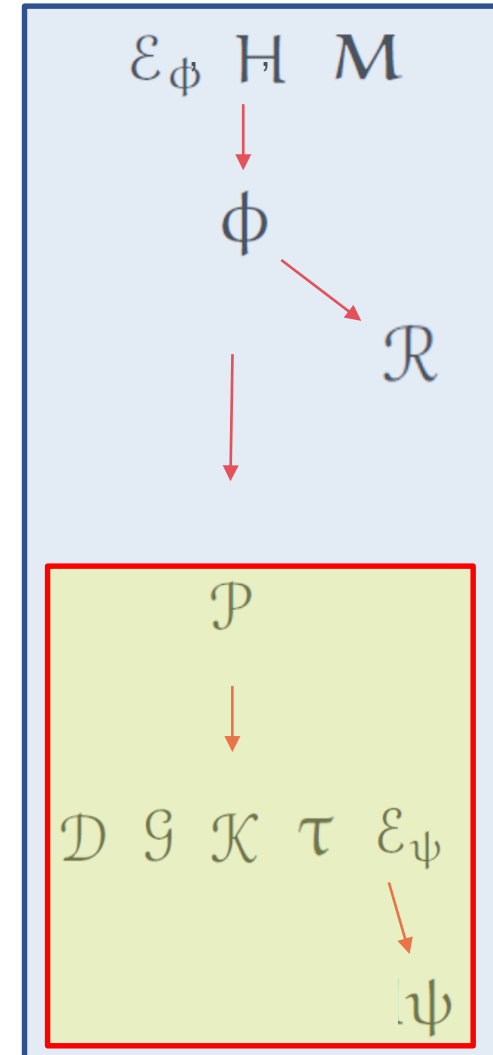
How far have we come?

Spatial operators

- Velocity expression
- Jacobian
- Mass matrix NE factorization
- Lyapunov equation for CRBs
- Mass matrix decomposition
- Riccati equation for ATBI
- Several operator identities
- Mass matrix Innovations factorization
- Mass matrix determinant
- Mass matrix inverse and factorization

Have started to build up a vocabulary of spatial operators that can be used to express and manipulate the structure of dynamics quantities.

*Now can see the rationale for the **algebra** part of SOA from the analytical transformations and simplifications possible using the operators.*



spatial operators family



Recursive Computational Algorithms

- $O(N)$ Gather and scatter recursions pattern
- $O(N)$ Body velocities scatter recursion
- $O(N)$ CRBs gather recursion
- $O(\mathcal{N}^2)$ mass matrix computation
- $O(N)$ NE scatter/gather inverse dynamics
- $O(\mathcal{N}^2)$ inverse dynamics based mass matrix
- $O(N)$ CRBs based inverse dynamics
- $O(N)$ ATBI gather recursion
- $O(\mathcal{N}^2)$ **forward dynamics**

Can derive such low-cost scatter/gather algorithms usually by examination of the spatial operator expressions.

Summary



- Introduced ATBI spatial operators
- Developed several operator identities
- Developed Innovations Factorization of the mass matrix
 - Has square and invertible factors
 - Can reduce forward dynamics costs
- Developed expression for inverse of factors
- Developed operator expression for the mass matrix inverse

SOA Foundations Track Topics (serial-chain rigid body systems)



1. **Spatial (6D) notation** – spatial velocities, forces, inertias; spatial cross-product, rigid body transformations & properties; parallel axis theorem
2. **Single rigid body dynamics** – equations of motion about arbitrary frame using spatial notation
3. **Serial-chain kinematics** – minimal coordinate formulation, hinges, velocity recursions, Jacobians; first spatial operators; $O(N)$ scatter and gather recursions
4. **Serial-chain dynamics** – equations of motion using spatial operators; Newton–Euler mass matrix factorization; $O(N)$ inverse dynamics; composite rigid body inertia; forward Lyapunov equation; mass matrix decomposition; mass matrix computation; alternative inverse dynamics
5. **Articulated body inertia** - Concept and definition; Riccati equation; alternative force decompositions
6. **Mass matrix factorization and inversion** – spatial operator identities; Innovations factorization of the mass matrix; Inversion of the mass matrix
7. **Recursive forward dynamics** – $O(N)$ recursive forward dynamics algorithm; including gravity and external forces; inter-body forces identity

SOA Generalization Track Topics



8. **Graph theory based structure** – BWA matrices, connection to multibody systems
9. **Tree topology systems** – generalization to tree topology rigid body systems, SKO/SPO operators, gather/scatter algorithms
10. **Closed-chain dynamics (cut-joint)** – holonomic and non-holonomic constraints, cut-joint method, operational space inertia, projected dynamics
11. **Closed-chain dynamics (constraint embedding)** – constraint embedding for graph transformation, minimal coordinate closed-chain dynamics
12. **Flexible body dynamics** – Extension to flexible bodies, modal representations, recursive flexible body dynamics



SOA Generalization Track Topics

1. **Graph theory based structure** – BWA matrices, SKO and SPO operators
2. **Tree topology systems** – generalization to tree topology rigid body systems, gather/scatter algorithms
3. **Operational space dynamics** – dynamics in task/constraint space, operational space inertia, decomposition and recursive computation
4. **Closed-chain dynamics (cut-joint)** – holonomic and non-holonomic constraints, cut-joint method, move and squeeze forces, projected dynamics
5. **Graph transformations** – Multibody topology transformation and decomposition, aggregation
6. **Closed-chain dynamics (constraint embedding)** – constraint embedding for graph transformation, minimal coordinate closed-chain dynamics
7. **Flexible body dynamics** – Extension to flexible bodies, modal representations, recursive flexible body dynamics
8. **Numerical methods and integrators** (Radu Serban) – ODE and DAE integration for multibody dynamics